



25th DAAAM International Symposium on Intelligent Manufacturing and Automation, DAAAM 2014

## Influence of Waviness and Vacancy Defects on Carbon Nanotubes Properties

Marino Brcic\*, Marko Canadija, Josip Brnic

*Faculty of Engineering, Department of Engineering Mechanics, University of Rijeka, Vukovarska 58, HR-51000 Rijeka, Croatia*

### Abstract

Previous and present theoretical and experimental research of polymer and other composites have shown that carbon nanotubes, acting as an reinforcements, significantly affect the final mechanical properties of aforementioned composites, thanks to its exceptional mechanical properties. However, the properties of carbon nanotube can be affected by the shape of nanotube, as well as various vacancy defects within the structure of carbon nanotube. Thus, the waviness and the vacancy defects decreases the final properties of nanocomposite structures. In this paper, the properties of straight and waved carbon nanotube are compared, on examples with different waviness factor, using the finite element method. Also, different vacancy defects are considered on the same straight and waved nanotube models.

© 2015 The Authors. Published by Elsevier Ltd. This is an open access article under the CC BY-NC-ND license (<http://creativecommons.org/licenses/by-nc-nd/4.0/>).

Peer-review under responsibility of DAAAM International Vienna

*Keywords:* carbon nanotube; waviness; vacancy defect

### 1. Introduction

Since the discovery of the carbon nanotubes [1], many researchers have attempted to find out their properties and characteristics, either experimentally [2 - 5] or theoretically [6 - 11]. A common conclusion is that carbon nanotubes possess extraordinary mechanical, thermal and electric properties, thus, they are a logical choice as an improvement in composite materials – nanocomposites, either to improve mechanical properties of composite, due to their extremely high tensile strength and elasticity modulus [12], or to improve electrical conductivity [13]. Because of their nano size, it is very difficult to conduct experimental studies of carbon nanotubes and nanocomposite materials,

\* Corresponding author. Tel.: +385-51-651-560; fax: +385-51-651-490.

*E-mail address:* [mbrbic@riteh.hr](mailto:mbrbic@riteh.hr)

therefore the computer multiscale modelling and numerical methods emerges as a logical solution. Considering numerical approaches, nanotubes have been modelled separately in two different systems of mechanics, molecular dynamics [8, 11, 14 - 16] and structural mechanics, which is based on the substitution of covalent bonds between the atoms with nodes and beam finite elements. Detailed overview and description of the modelling of nanotubes and multiscale modelling methods of nanocomposites is given in author's previous works [17 - 19]. The reader is referred to these publications, thus in this paper the attention will not be dedicated to the modelling of carbon nanotubes.

Most of the research on mechanical properties of carbon nanotubes are conducted on ideal model of nanotube [20 - 23]. But carbon nanotubes rarely come in ideal form. They are usually waved, regardless of the manner of production control [24, 25]. Studies have shown that the waviness of the nanotube has an influence on the final mechanical properties of nanocomposite materials [26 - 28]. Also, a common problem in nanotube structure is appearance of vacancy defects [29, 30], which can occur either naturally, i.e. rehybridization, or artificially. It is, therefore, very interesting to study the impact of vacancies and waviness of nanotubes on their mechanical properties, specifically on the elastic modulus, because it eventually leads to decrease of final mechanical properties of nanocomposites. Change of elastic moduli of the carbon nanotube is given in this paper, shown on several examples of carbon nanotubes, with different waviness and vacancy defects.

## 2. Waviness and vacancy defects

As mentioned before, the carbon nanotubes as a reinforcement in the composite materials significantly affect the final mechanical properties of the nanocomposites, due to its exceptional properties. However, in several papers [31, 32] only the slightly improvement of the nanocomposite properties, reinforced with the carbon nanotubes, has been reported. The reason for this is weak load transfer from the composite matrix to the reinforcement, or better said, weak bond between matrix and the reinforcement, i.e. nanotube, since this bond is established through weak van der Waals bonds [33, 34]. Additional reasons are the waviness of carbon nanotubes and appearance of various defects in nanotube structure.

Experiments have shown that carbon nanotubes within nanocomposites are mainly waved [35, 36]. This can be explained by the fact that nanotubes have very small bending stiffness, due to large aspect ratio, i.e. diameter in order of nanometers and length in order of micrometer. Waviness of the nanotube is in the literature defined with the waviness ratio  $w$  [37]:

$$w = \frac{a}{l} \quad (1)$$

where  $a$  represents wave amplitude and  $l$  wavelength, as shown in Fig. 1.

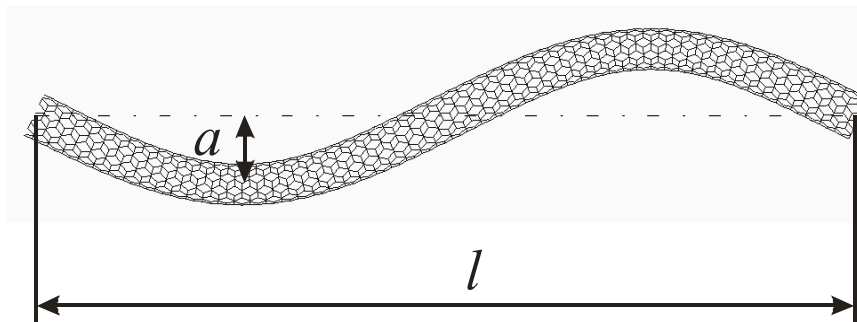


Fig. 1. Definition of the waviness ratio of the nanotube.

Apart from waviness, various defects, such as vacancies, metastable atoms, pentagons, heptagons, heterogeneous atoms, distortion, etc. [38, 39] can appear inside nanotube structure. Vacancies, or missing atoms, greatly reduce

strength of the nanotube. Such defects can occur due to the ionic radiation, absorption of electrons or specific production method [40].

### 3. Examples and results

Influence of waviness and vacancy defects on elastic modulus of carbon nanotube in this paper is shown on finite element model of single walled carbon nanotube, armchair (5, 5) pattern, with diameter 0,679 nm and aspect ratio (length/diameter) 20,2. The nanotube is modelled as a space frame structure, where the atoms are replaced with nodes, and covalent bond with beam finite elements [17 - 19]. There are 1120 nodes and 1670 beam elements in one model of nanotube.

An axially loaded cantilever nanotube model was used to determine the elastic modulus, and 1 nN axial force was used in all examples. The longitudinal elastic modulus was obtained using classical term:

$$E = \frac{F \cdot l}{A \cdot \Delta l} \quad (2)$$

where  $l$  represents nanotube length (13,65 – 13,7 nm),  $A$  is nanotube's cross section area (0,715 nm<sup>2</sup>), and  $\Delta l$  longitudinal elongation.

In relation to term (1), five models of nanotube have been prepared, with different waviness ratio, i.e. four waved nanotube and one straight ( $w = 0$ ), as shown in Fig. 2. Waved shape of nanotube was prepared using eigenvalue analysis, with different eigenvalue parameters.

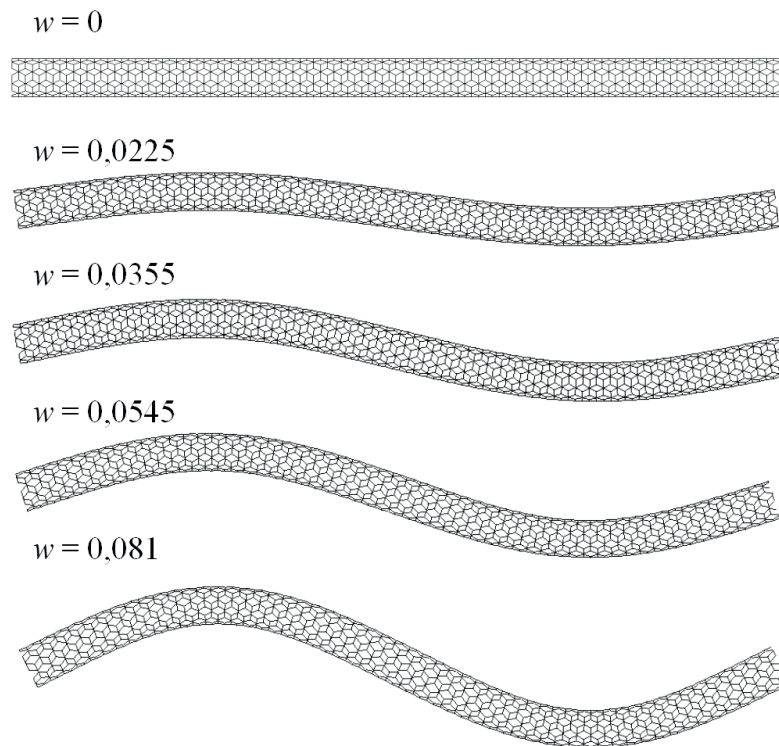
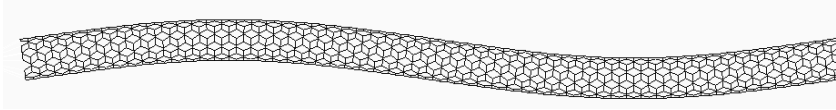


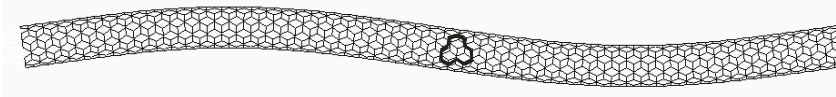
Fig. 2. Examples of waved nanotubes.

Vacancies in nanotube model are obtained by deleting one node and three beam elements from structure. Three different cases of vacancy defects have been prepared, as follows. In first case the vacancies are prepared as shown in Fig. 3., to show the change of elastic modulus versus position of the vacancy.

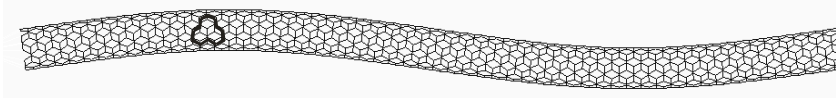
- no vacancy;



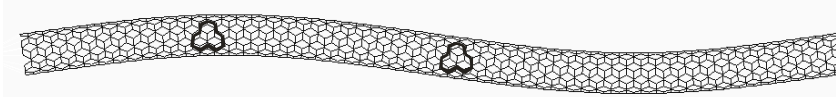
- one central vacancy;



- one side vacancy;



- two vacancies, side and central;



- two side vacancies;

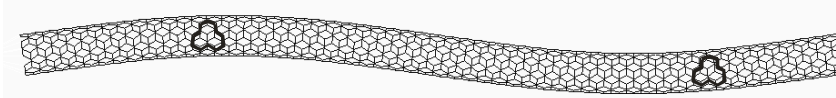


Fig. 3. Vacancy layout in carbon nanotube.

In addition to first case, in the second vacancy case, the given percentage of randomly selected atoms, i.e. nodes (0,1%, 0,5%, 1%, 2%, 5% and 10%) were removed from the nanotube structure. Since vacancies are one of the reason of nanotube waviness, another case of vacancy defects is presented, in which 1 to 8 atoms were removed from the position with maximum curvature at the internal side of the carbon nanotube, Fig. 4. The remaining part of the nanotube is defect free. The latter vacancy defect case was implemented only on the model with waviness ratio 0,0545.

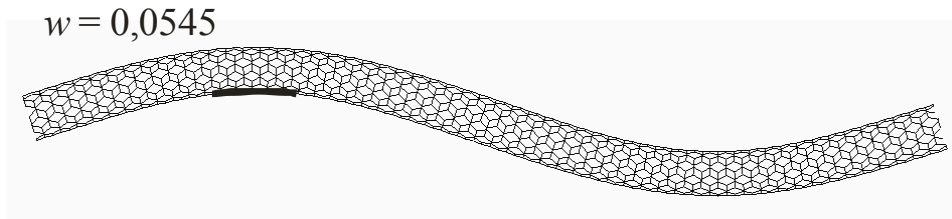


Fig. 4. Position of 1 to 8 vacancy defect in waved nanotube, marked with black line.

Obtained results for longitudinal elastic modulus are given in tables 1 and 2, and in Fig. 5., for corresponding vacancy case. As expected, there is notable drop in elastic modulus value with the increase of the waviness of nanotube. On the other hand, value of elastic modulus also decreases with the increase of the vacancies (from 0,1% to 10%) within the same waviness ratio of the nanotube.

Table 1. Results for first vacancy case.

Vacancy:	Longitudinal elastic modulus $E$ , GPa				
	Waviness ratio, $w$ :				
	0	0,0225	0,035	0,0545	0,081
No vacancy	1069,42	530,24	187,05	126,36	86,75
1 central vacancy	1040,51	515,91	185,95	125,53	85,21
1 side vacancy	1040,51	515,91	186,50	125,86	85,21
2 vacancies, central and side	1018,49	513,14	185,77	125,36	84,83
2 side vacancies	1018,49	513,14	185,68	125,39	84,94

Table 2. Results for second vacancy case.

Vacancy percentage:	Longitudinal elastic modulus $E$ , GPa				
	Waviness ratio, $w$ :				
	0	0,0225	0,035	0,0545	0,081
0,1%	1040,51	525,85	183,45	121,52	82,267
0,5%	997,38	534,69	163,06	121,52	79,52
1%	912,29	420,45	175,03	112,23	82,26
2%	844,27	420,45	157,67	102,03	74,55
5%	585,09	329,68	106,58	62,97	53,61
10%	185,09	167,44	23,67	33,53	7,18

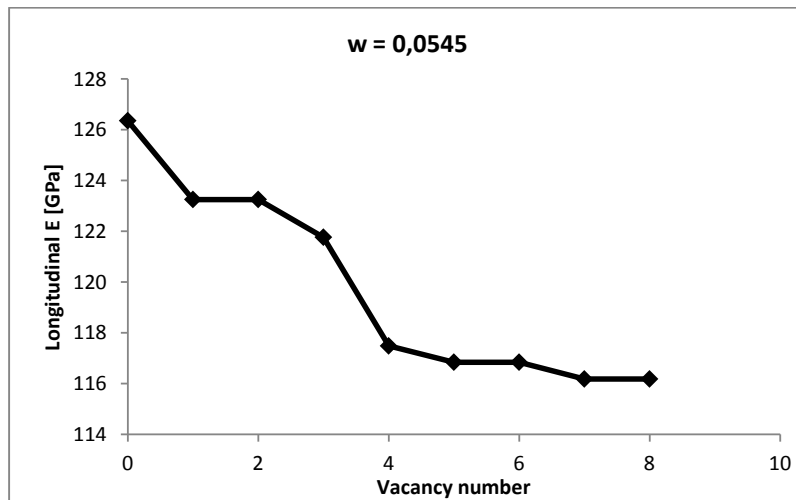


Fig. 5. Results for third vacancy case.

## Conclusion

Carbon nanotubes are logical and quality choice as a reinforcement in the nanocomposite materials, due to their excellent mechanical properties. However, because of various causes during production, as well as the geometric characteristics, they come in waved form, with a variety of defects in the structure. Waviness and defects greatly reduce their properties, which ultimately leads to a small improvement of final mechanical properties of nanocomposites. Influence of aforementioned imperfections on nanotube properties, is shown on change of elastic modulus of finite element model of carbon nanotube, with different waviness ratio and different vacancy defects. Thus, the longitudinal elastic modulus of the straight carbon nanotube decreases with increase of the waviness ratio, which is most pronounced in the nanotubes without defects (from 1069 GPa to 86 GPa, 92%). Small decline of elastic modulus is noticeable with the increase of vacancies in the nanotubes with same waviness ratio, from Tab. 1, but with drastic increase of vacancies, a drastic decrease of elastic modulus, within nanotubes with same waviness ratio, can be noticed (Tab. 2.). Irregularities in values of elastic modulus in Tab. 2. can be attributed to randomly positioned vacancies in each particular example, i.e. analysis. Fig. 5. shows change of elastic modulus if vacancies accumulate on specific position in nanotube structure. It should also be noted that values of elastic modulus match in the examples with the same waviness ratio and the same number of vacancies, and from the examples with 1 or 2 vacancies it is possible to conclude that position of the defect doesn't affect the elastic modulus (Tab. 1.).

## Acknowledgements

This work has been fully supported by the University of Rijeka under the project 13.09.1.1.01, and by Croatian Science Foundation under the project no. 6876 – Assessment of structural behavior in limit state operating conditions. This support is gratefully acknowledged.

## References

- [1] S. Iijima, Helical microtubules of graphitic carbon, *Nature* 354 (1991), 56.
- [2] M.M.J. Treacy et al, Exceptionally high Young's modulus observed for individual carbon nanotubes, *Nature* 381 (1996), 678-680.
- [3] S. Xie, et al, Mechanical and physical properties on carbon nanotube, *Journal of Physics and Chemistry of Solids*, 61 (2000), 1153-1158.
- [4] Wong EW, Sheehan PE, Lieber, CM (1997) Nanobeam Mechanics: Elasticity, Strength, and Toughness of Nanorods and Nanotubes. *Science* 26:1971-1975.
- [5] Yu M, Lourie O, Dyer MJ, Moloni K, Kelly TF, Ruoff RS (2000) Strength and Breaking of Multiwalled Carbon Nanotubes Under Tensile Load. *Science* 28:637-640.
- [6] J.P. Lu, Elastic Properties of Carbon Nanotubes and Nanoropes, *Phys. Rev. Lett.*, 79 (1997), 1297-1300.
- [7] R.S. Ruoff et al, Mechanical properties of carbon nanotubes: theoretical predictions and experimental measurements, *Comptes Rendus Physique*, 4 (2003), 993-1008.
- [8] B.I. Yakobson, M.P. Campbell, C.J. Brabec, J. Bernholc, High Strain Rate Fracture and C – Chain Unraveling in Carbon Nanotubes, *Computational Materials Science* 8 (1997), 341-348.
- [9] J. Bernholc, C. Brabec, M. Buongiorno Nardelli, A. Maiti, C. Roland, B.I. Yakobson, Theory of Growth and Mechanical Properties of Nanotubes, *Applied Physics A* 67 (1998), 39-46.
- [10] G. Overney, W. Zhong, D. Tomanek, Structural Rigidity and Low Frequency Vibrational Modes of Long Carbon Tubules, *Zeitschrift fur Physik D* 27 (1993), 93-96.
- [11] S. Iijima, C. Brabec, A. Maiti, J. Bernholc, Structural Flexibility of Carbon Nanotubes, *Journal of Chemical Physics* 104 (1996), 2089-2092.
- [12] K.I. Tserpes, P. Papanikos, G. Labeas, S.G. Pantelakis, Multi – scale Modeling of Tensile Behaviour of Carbon Nanotube Reinforced Composites, *Theoretical and Applied Fracture Mechanics* 49 (2008), 51-60.
- [13] M. Murarescu, D. Dima, G. Andrei, A. Circiumaru, Influence of MWCNT dispersion on electric properties of nanocomposites with polyester matrix, *Annals of DAAAM for 2011 & Proceedings of 22nd International DAAAM Symposium*, 22 (2011), 925-926.
- [14] T. Chang, H. Gao, Size – dependent Elastic Properties of a Single – Walled Carbon Nanotube Via a Molecular Mechanics Model, *Journal of the Mechanics and Physics of Solids* 51 (2003), 1059-1074.
- [15] K.M. Liew, C.H. Wong, M.J. Tan, Tensile and Compressive Properties of Carbon Nanotube Bundles, *Acta Materialia* 54 (2006), 225-231
- [16] Y. Zhang, H. Huang, Stability of Single – Wall Silicon Carbide Nanotubes – Molecular Dynamics Simulation, *Computational Materials Science* 43 (2008), 664-669.
- [17] M. Brcic, M. Canadija, J. Brnic, FE modeling of a multi-walled carbon nanotubes, *Estonian Journal of Engineering*, 15 (2009), 79-86.

- [18] M. Brcic, M. Canadija, J. Brnic, A finite element model for thermal dilatation of carbon nanotubes, *Review on Advanced Materials Science*, 33 (2013), 1-6.
- [19] M. Brcic, M. Canadija, J. Brnic, Estimation of material properties of nanocomposite structures, *Meccanica*, 48 (2013), 2209-2220.
- [20] Li C, Chou TW (2003) A Structural Mechanics Approach for the Analysis of Carbon Nanotubes. *International Journal of Solids and Structures* 40:2487-2499.
- [21] Li C, Chou TW (2004) Modeling of Elastic Buckling of Carbon Nanotubes by Molecular Structural Mechanics Approach. *Mechanics of Materials* 36:1047-1055.
- [22] Li C, Chou TW (2003) Elastic Moduli of Multi – Walled Carbon Nanotubes and the Effect of van der Waals Forces. *Composites Science and Technology* 63:1517-1524.
- [23] A.L. Kalamkarov, A.V. Georgiades, S.K. Rokkam, V.P. Veedu, M.N. Ghasemi-Nejhad, Analytical and Numerical Techniques to Predict Carbon Nanotubes Properties, *International Journal of Solids and Structures* 43 (2006), 6832-6854.
- [24] J.N. Ginga et al, Waviness reduces effective modulus of carbon nanotube forests by several orders of magnitude, *Carbon*, 66 (2014), 57-66.
- [25] S. Bal, S.S. Samal, Carbon nanotube reinforced polymer composites – a state of the art, *Bulletin of Materials Science*, 30(4) (2007), 379-386.
- [26] F. T. Fisher et al, Effects of nanotube waviness on the modulus of nanotube – reinforced polymers, *Applied Physics Letters*, Vol. 80 (2002), 4647-4649.
- [27] F.T. Fisher, R.D. Bradshaw, L.C. Brinson, Fiber waviness in nanotube-reinforced polymer composites-i: Modulus predictions using effective nanotube properties, *Composites Science and Technology* 63 (2003), 1689–1703.
- [28] R.D. Bradshaw, F.T. Fisher, L.C. Brinson, Fiber waviness in nanotube-reinforced polymer composites-ii: Modeling via numerical approximation of the dilute strain concentration tensor, *Composites Science and Technology* 63 (2003), 1705–1722.
- [29] J. Charlier, Defects in carbon nanotubes, *Accounts of Chemical Research* 35 (2002), 1063–1069.
- [30] T. Ebbesen, T. Takada, Topological and {SP<sup>3</sup>} defect structures in nanotubes, *Carbon* 33 (1995), 973 – 978.
- [31] D. Qian et al, Mechanics of Carbon nanotube, *Appl. Mech. Rev.*, 55 (2002), 495-533.
- [32] P.M. Ajayan et al, Single – Walled Nanotube – Polymer Composites: Strength and Weaknesses, *Adv. Mater.*, 12 (2000), 750-753.
- [33] H. Tan et al, The effect of van der Waals – based interface cohesive law on carbon nanotube – reinforced composite materials, *Composites Science and Technology*, 67 (2007), 2941-2946.
- [34] L.Y. Jiang, Y. Huang, H. Jiang, G. Ravichandran, H. Gao, K.C. Hwang, B. Liu, A cohesive law for carbon nanotube / polymer interfaces based on the van der Waals force, *Journal of the Mechanics and Physics of Solids*, 54 (2006), 2436-2452.
- [35] M.S.P. Shaffer, A.H. Windle, Fabrication and Characterization of Carbon Nanotube / Poly (vinyl alcohol) Composites, *Adv. Mater.*, 11 (1999), 937-941.
- [36] B. Vigolo et al, Macroscopic Fibers and Ribbons of oriented Carbon Nanotubes, *Science*, 290 (2000), 1331-1334.
- [37] M. Farsadi et al, Numerical investigation of composite materials reinforced with waved carbon nanotubes, *Journal of Composite Materials*, 0 (2012), 1-10.
- [38] F. Banhart, Irradiation effects in carbon nanostructures, *Reports on Progress in Physics*, 62 (1999), 1181.
- [39] S. Iijima et al, Pentagons, heptagons and negative curvature in graphite microtubule growth, *Nature*, 356 (1992), 776-778.
- [40] W. Hou, S. Xiao, Mechanical Behavior of Carbon Nanotubes with Randomly Located Vacancy Defects, *Journal of Nanoscience and Nanotechnology*, 7 (2007), 1-8.