

## KEYHOLE FORMATION DURING LASER WELDING

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**Abstract:** In this paper a short description of the keyhole effect in case of laser welding is made. Several aspects of the properties of the keyhole and the influence over the weld bead are considered. The geometry of the weld bead of austenitic stainless steel is also investigated.

**Key words:** Laser welding, keyhole, austenitic stainless steel

### 1. INTRODUCTION

Laser beam welding is a welding technique used to join multiple pieces of metal through the use of a laser. The beam provides a concentrated heat source, allowing for narrow, deep welds and high welding rates. The process is frequently used in high volume applications, such as in the automotive industry.

An important mechanism in laser beam welding is the interaction of the laser beam with the material. This interaction mechanism is influenced by many parameters such as: the laser power  $P$ , the intensity distribution  $I$  of this power at the surface, the welding speed  $v$ , the material properties and the wavelength of the laser radiation  $\lambda$ .

### 2. KEYHOLE EFFECT

In order to perform the welding process, the minimum energy needed is of  $10^6$  W/cm<sup>2</sup> where the diameter of the beamer represents 30% of the part thickness.

The diameter of the laser beam used for the welding process generally varies between 0.2...1 mm, with a reference value of 0.3 mm. For the geometry of the elements, usually the lap joint is used, and only seldom the add-on material. Lap welds melt a lot of metal to produce a small connection, but they have a much larger tolerance on position than butt welds (Pascu et al., 2009, a). As relative motion between the beam centerline and material occurs, the molten metal flows around from the front of the keyhole and solidifies at the back, forming a laser weld (Fig. 1). By traversing the beam relative to the workpiece, a narrow weld bead is formed with a high aspect ratio (depth/width), illustrated in Fig. 2. (John, 2005)

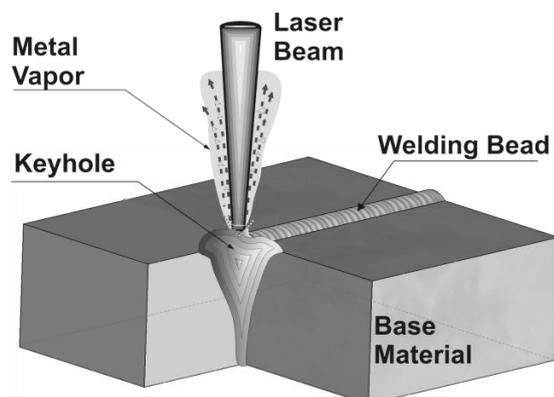


Fig. 1. Schematic of the keyhole effect

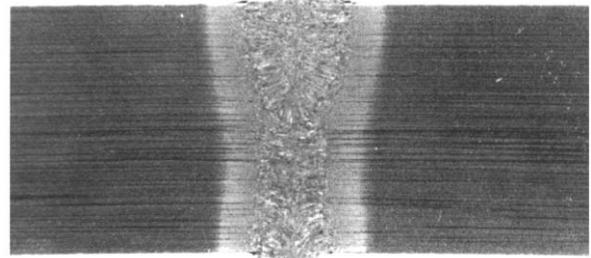


Fig. 2. Transverse section through a full penetration keyhole weld made in a carbon-manganese steel of thickness 6mm using an Nd: YAG laser beam

The keyhole phenomena induce in metal bath an irradiation effect which will provide the energy needed to vaporize the base material. The heat transfer process at the interface between the solid-liquid phase involves besides the thermal conduction also the convection effect due to the movement of the melted metal into the metal bath. Only the vapour presence combined with thermal conduction and convection effect will provide a deep penetration of the welding. In laser welding the keyhole effect produces two major consequences:

- The energetic transfer between the laser radiation and the material is higher because the laser radiation is propagated through the keyhole channel and it is absorbed directly inside the material.
- The heat source will generate sudden variation in time and space of the material temperature and powerful evaporation will occur. The rapid vaporisation will generate an increasing pressure which facilitates the process transformation of liquid metal into vapour.

The hot gas escaping from the keyhole forms a plasma or plume above the workpiece. The laser beam energy is absorbed on the walls of the keyhole (Vught, 2003). The keyhole effect allows welding procedures with deep diffusion due to the fact that the laser beam heat is well absorbed in a steamy medium. The reflectivity of the metal is only important until the keyhole weld begins. After forming the first drop of melted metal, the level of absorbed energy will increase because the metallic bath has a low reflection degree, causing the temperature to significantly increase up to the point where metal steams form (Pascu et al., 2009, b).

The laser beam is focused to produce an incident power at the surface of the material; power which will initialize the vaporisation and the formation of the keyhole effect. Keyhole welding is dependent on focused spot power density (laser power and focused spot size), welding speed, material, melting temperature, material reflectivity, material conductivity, and the like. In general, CW keyhole welding of steels and stainless steels is possible above 600 watts. For materials such as aluminum and copper, keyhole welding is generally not possible in the CW range below 1000 Watts (Havrilla, 1999).

The main characteristic of the laser welding is the quick solidification of the metal bath. During this cooling, the material

contracts, creating tensile stresses in the fusion zone. When using short welding intervals (5 ms), the welding belt might crack. It is possible the laser influenced areas of high-alloyed steel, turn into martensite with major drawbacks for the welding. These drawbacks can be avoided by increasing the welding intervals or by a local preheating procedure. Another wide spread method used for obtaining high quality welding results consists in using the shield gas for preventing the oxidation of the metal bath (Pascu et al., 2009).

### 3. EXPERIMENTAL PROCEDURE

The study is concerned to analyze the welding behaviour of stainless steel 304. Austenitic Cr-Ni stainless steel has a good corrosion resistance, high ductility, excellent drawing, forming, and spinning properties. Essentially non-magnetic, becomes slightly magnetic when cold worked. Low carbon content means less carbide precipitation in the heat-affected zone during welding and a lower susceptibility to intergranular corrosion. For the achievement of the welding tests, a 3,3 kW Nd:Yag continuous wave laser was used as a thermal source together with an ABB 6-axes robot and a coaxial cladding unit made by Rofin. The welding parameters were varied in order to study the geometry and the manner in which a weld bead is constituted. The penetration depth in laser welding is proportional to the power density of the laser beam and is incident function between the focal spot size and its power. The values of the welding regime used for the experiments are presented in table 1.

Sample code	Spot diameter [mm]	Laser power [W]	Power density [W/cm <sup>2</sup> ]	Welding speed [mm/s]
1.1.	0,5	700	356,688	20
1.2.	0,5	900	458,599	40
1.3.	0,5	1100	560,51	60

Tab. 1. Welding parameters for the test pieces

### 4. RESULTS AND COMMENTS

All the samples were prepared for analyses using grit paper, alumina and chemical etched with royal water in a molar ratio of 1:3.

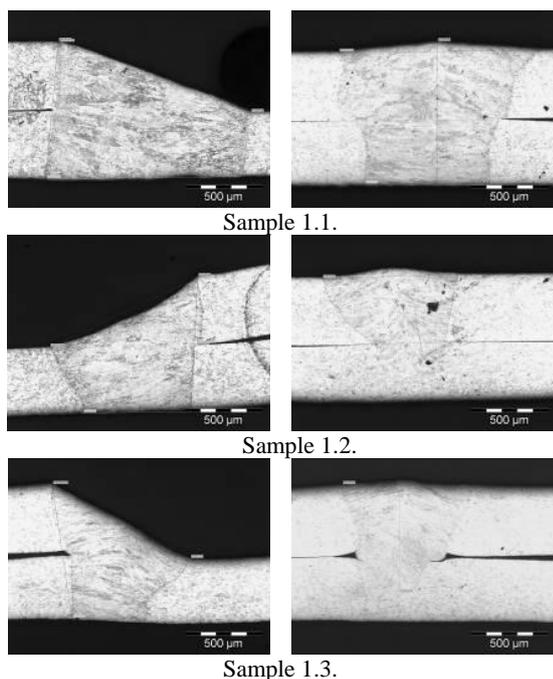


Fig. 3. Section of welding tracks; left: fillet, right: overlapp

The behavior of the weld bead in case of fillet and overlapp welding is clearly visible in figure 3. The speed has a major influence over the penetration and the width of the weld. Even so the power used at sample 1.1 is smaller the width of the bead is higher and a full penetration was achieved. Also at sample 1.1 a straight ideal geometry of the bead was obtained. In case of a higher speed at sample 1.2 and 1.3 a smaller width of the weld can be observed and also only a partial penetration was achieved. The penetration of the overlap samples is proportionally inverse with the laser power and the welding speed. The penetration is linearly decreasing if the welding speed is higher. Also the width of the welding bead is smaller in case of a high speed. In table 2 are presented the values of the penetration and width of the analysed samples.

Sample code	Penetration [µm]		Width [µm]	
	fillet	overlapp	fillet	overlapp
1.1.	-	928	1280	1310
1.2.	-	730	705	880
1.3.	-	732	482	852

Tab. 2. Aspects highlighted in the case of the welded samples

### 5. CONCLUSION

The irradiation of the metal bath is influenced by the convergent or divergent propagation of the laser beam. In case of Nd: YAG laser the absorption takes place through the Fresnel reflection which appears at the top of the metal bath and inside the keyhole. During the formation and evolution of the keyhole the laser beam irradiates the front wall of the keyhole and the position of the beam becomes relatively off-axis with the keyhole channel. Also as welding speed increases the process becomes successively more dominated by direct absorption at the keyhole walls.

The quantity of absorbed energy through Fresnel reflection depends on the incident angle of the radiation over the metal bath. This study will provide the necessary data for the further research in which the behaviour of black and white welding will be investigated.

### 6. ACKNOWLEDGEMENTS

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