



## EFFECT OF HIGH FEED MILLING ON THE MICROSTRUCTURE AND MICROHARDNESS OF SURFACE LAYER

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**Abstract:** The paper is dealing by the evaluation of microstructure and microhardness of surface layer after high feed milling. The quality of surface layer is one of the main important outputs of cutting process. Experiment was realized on the universal 5 axis CNC cutting centre, like testing cutting tool material was used high alloy high speed steel ASP 2023 Cutting speeds and cutting feed rates were variable parameters and cutting depth was constant parameter. Study of surface layer properties helps to evaluate influence of machining.

**Key words:** machining, microhardness, surface layer, microstructure, high feed milling

### 1. INTRODUCTION

High feed machining is a difficult term to define due to a number of decisive factors including the properties of the material being machined, the availability of suitable tool materials, wide range of speeds and feeds of available machine tools (Erdel, 2003).

High speed machining reaches increase in material removal, quality of machined surface and life of a tool by the significant increase of cutting speed with decreased cross section of a shaving and lowered cutting force (Shaw, 2005).

High relative speed of the shaving with respect to the front area of a tool, together with the new quality of a cutting edge, increases the cutting process amount of heat, which is removed with the shaving, lowers heat and mechanical loading on the tool and increases its useful life. Reduction of heat flows that go into the tool, frame of a machine and the machined part gives us increase in the machined part accuracy and quality of its surface (Grzesik, 2008).

### 2. MACHINE TOOL, MATERIAL AND CUTTING PARAMETERS

For experimental work was used a cutter from the Kennametal Europe GmbH company. The cutter F3AJ1800ADN30 is a carbide three cutting edges shank cutter with the diameter 18 mm and helix rise of 30°. This cutter is suitable for high speed machining due to its rigid body and design with satisfactorily large tooth gap.

The tool is also suitable for finish cutting. Primarily the cutter is intended for machining of P, M, K and S materials, and alternatively for machining of N materials.

The material for experimental part was select ASP 2032 with following specification in table 1.

| Elements   | C    | Cr  | Mo  | W   | Co | V   |
|------------|------|-----|-----|-----|----|-----|
| Weight [%] | 1,28 | 4,1 | 5,0 | 6,4 | -  | 3,1 |

Tab. 1. Specification of material ASP 2032

ASP 2023 is a high alloy high speed steel, manufactured powder metallurgically using the ASP Process. Material ASP 2023 is suitable for operations under extremely demanding

conditions. Material ASP 2023 can be work as follows: machining; polishing; plastic forming; electrical discharge machining; welding.

Delivery hardness was supplied soft annealed max. 260 HB. Heat in a protective atmosphere to 850-900°C, hold for 3 hours, slow cool at 10°C/h down to 700°C, then air cooling.

For the experimental work was tested hardness HBW 2.5/187.5 of material in the Vitkovice testing center (VTC.30) with hardness tester EmcoTest. At drafting measurement of hardness was proceeded from standard for hardness test of Brinell CSN EN ISO 6506.

The microstructure evaluation of basic material was effected on luminous metallographical microscope NEOPHOT 21 at 500x magnification. Figure 1 shows secondary carbides in temper martensite base of material ASP 2023.

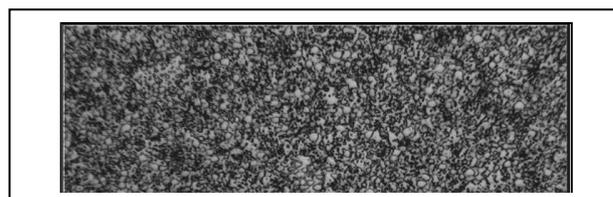


Fig. 1. The metallographical detail of material ASP 2023 (magnified 500x, etching agent Nital 1%)

The major variable in the experiment are cutting conditions. The axial cutting depth was determined with regard to application of this technology during finish to:

- Cutting depth  $a_p = 0.25$  mm,
- Effective width of cuts  $a_e = 16$  mm,
- Diameter of milling cutter  $D = 18$  mm,
- Feed on the tooth  $f_z = 0.33$  mm.

The following cutting conditions were chosen for experimental work on the universal 5 axis CNC cutting centre Deckel Maho:

- Feed rates  $v_f$  10, 15, 20  $\text{m}\cdot\text{min}^{-1}$ ,
- Revolutions  $n$  10000, 15000, 20000  $\text{min}^{-1}$ ,
- Cutting speeds  $v_c$  565.5, 848.2, 1131.0  $\text{m}\cdot\text{min}^{-1}$ .

### 3. MEASUREMENT OF SURFACE MICROHARDNESS

The measurement of surface microhardness HV0.1 was done on a automatic measuring apparatus – the AM 43 LECO hardness tester in the Mechanical laboratory of the Faculty of Mechanical Engineering of VŠB-Technical University of Ostrava. The load of the measuring was 100 g.

The indenter was the Vickers diamond pyramid. Measured values of depths of hard layer  $h_z$  refer that during the cutting speed approximately  $v_c$  565.5  $\text{m}\cdot\text{min}^{-1}$  (feed rate  $v_f$  10  $\text{m}\cdot\text{min}^{-1}$ ) the widest depths of hard layer  $h_z$  were achieved. The depth of hard layer improves when we exceed this speed.

The narrowest depths of hard layer  $h_z$  are of course achieved during the cutting speed  $v_c$  1131.0 m.min<sup>-1</sup> (feed rate  $v_f$  20 m.min<sup>-1</sup>). Figure 2 shows the photograph of comprehensive view of the machined surface 2. Cutting conditions for surface 2 were select: feed rate  $v_f$  15 m.min<sup>-1</sup>, revolution  $n$  15000 min<sup>-1</sup>, cutting speed  $v_c$  848.2 m.min<sup>-1</sup>.



Fig. 2. The sample of machined surface 2 (magnified 200x, etching agent Nital 1 %)

#### 4. INFLUENCE OF CUTTING PARAMETERS ON MICROHARDNESS MACHINED SURFACE

The widest depths of hard layer  $h_z$  were achieved at cutting speed  $v_c$  565.5 m.min<sup>-1</sup> ( $v_f$  10 m.min<sup>-1</sup>). The depth of hard layer is lower with increasing cutting speed.

Figure 3 shows influence of cutting parameters on microhardness values of material ASP 2023 for three machined surface, that is:

- Surface 1 (feed rate  $v_f$  10 m.min<sup>-1</sup>, revolution 10000 min<sup>-1</sup>, cutting speed  $v_c$  565.5 m.min<sup>-1</sup>),
- Surface 2 (feed rate  $v_f$  15 m.min<sup>-1</sup>, revolution 15000 min<sup>-1</sup>, cutting speed  $v_c$  848.2 m.min<sup>-1</sup>),
- Surface 3 (feed rate  $v_f$  20 m.min<sup>-1</sup>, revolution 20000 min<sup>-1</sup>, cutting speed  $v_c$  1131.0 m.min<sup>-1</sup>).

Depth mark of measuring 1 was measured in half of hard layer machined surface. Other values of microhardness HV0.1 (depth mark of measuring 2 up to 10) were continuous measured with measuring pitch 250  $\mu$ m in the depth of material in vertical direction on surface.

Improvement in the microhardness values were demonstrated during high speed machining. The mentioned theoretical assumptions were confirmed (Skopec ek & Vodi ka, 2005).

Material microhardness declines with increased cutting speed (feed rate) to the feed rate values around  $v_f$  10 to 20 m.min<sup>-1</sup> and then remains constant.

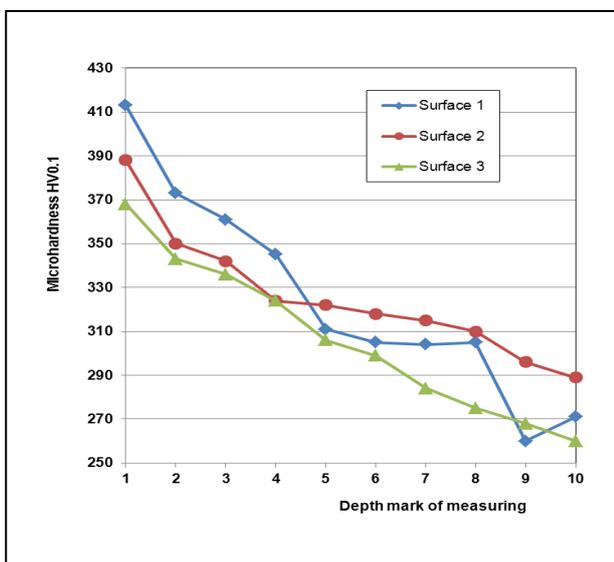


Fig. 3. The microhardness values of material ASP 2023 for variables cutting parameters of high feed cutting

During cutting with the three-teeth cutter the highest microhardness values were achieved at cutting speed  $v_c$  565.5 m.min<sup>-1</sup> (feed rate  $v_f$  10 m.min<sup>-1</sup>), on the other way, the lowest microhardness values were achieved during cutting with the cutting speed  $v_c$  1131.0 m.min<sup>-1</sup> (feed rate  $v_f$  20 m.min<sup>-1</sup>).

#### 5. CONCLUSION

The results of the experiments imply that introduction of high feed milling will result in significant time savings of the milling, and additional finishing of the machined surface will be eliminated with concurrent drop of production costs.

This experiment brings advances in cutting technology and helps to manufacturing companies lower costs, shorten delivery times, high quality parts and so on.

Similar results were achieved also in the works (Danišová & Majerík, 2009), (Dobr anský & Mandul ak 2008) and (Ru arovsk y, Velišek & Koř al, 2008) in the frame of design and planned experiments in the manufacturing of mechanical engineering.

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