



## ON THE REAMING OF AUSTENITIC STEELS WITH COATED CERMETS

PISKA, M[iroslav] & SLANY, M[artin]

**Abstract:** High effective cermet reaming of austenitic steel with cutting speeds 40-100 m/min, feed per revolution 0.2-0.8 mm and flood cooling has been analysed. A CNC machining sequence including solid carbide drilling, a semi-finishing carbide boring and cermet reamer finishing of the stainless steel AISI 316L were used and analysed. The results show a very effective cutting with surface roughness  $R_a$  below 1.0  $\mu\text{m}$ , with high accuracy of IT 5 and convenient specific energy.

**Key words:** reaming, austenite, cermet, cooling, nanocomposite

### 1. INTRODUCTION

In the second half of the 20th century monolithic cutting tools were replaced with so-called indexable inserts and the reaming heads were innovated with several brazed cutting edges and guiding parts. The new designs helped to produce very effective cutting tools at reasonable prices. The producers of precise tools today have to design cutting tools with a quick exchange that guarantee a high production dimensional stability and consistent high quality as well as consistent high quality. A new strategy for reaming with minimum quantity lubrication (MQL) has been studied recently (De Chiffre et al., 2008-9) with an excellent dimensional and quality evaluation (Muller, 2009). New cermet reamers have been studied quite recently (Slany, 2011). The basic advantages of the finishing tools can be high-lighted as follows:

- the reamers are particularly recommended for reaming materials with tensile strength ranging from 400 MPa to 1000 MPa;
- the tools prevail with high productivity due to high cutting speed from 100 up to 240 m/min (4-10 times higher than standard carbide reamers);
- a good surface quality, shape and diameter accuracy is produced for steels with tensile strength below 600 MPa;
- a smooth roughness (surface quality is improved by high stiffness of cermet head and carbide shank with high Young's module);
- chips are intensively removed from the cutting edge by means of coolant flow through inner channels;
- high stability of the manufacturing process and life time due to no affinity with machined material;
- high performance/price ratio – due to reduction of WC and substitutions of TiN, TiC and Ti(C,N) phases,
- advanced design of the modern reamer heads as an assembly set makes it very competitive due to a delivery time of 24 hours from the producer to the user.

### 2. THEORY OF FINISHING WITH REAMERS

According to the ISO 3002-4 cutting design (3 cutting flutes and 3 guides) - Fig. 1 - the reamer head is loaded with several normal and tangential force components, resulting in two measurable variables – thrust force  $F_f$  and torque moment  $M_t$ , integrating all the contributions from the cutting and interface friction:

$$F_f = \sum_{i=1}^z F_{fi} + \sum_{i=1}^g F_{Ai} \quad (1)$$

$$M_t = \sum_{i=1}^z M_{ci} + \sum_{i=1}^g M_{fi} \quad (2)$$

where the first members in the equations represent mainly the cutting parts and the second the passive (friction) shares. The individual torque moments can be derived from the instantaneous forces and appropriate radii. The other useful variable - specific energy of reaming - can be simplified to equation (3), where parameters of chip-cross section and cutting conditions are also included:

$$e_{ci} = \left( \frac{M_{ci} \cdot n}{9.55} + \frac{F_{fi} \cdot n \cdot f}{6 \cdot 10^4} \right) \cdot \frac{120}{\pi \cdot n \cdot f \cdot a_p \cdot (D - a_p)} \quad (3)$$

### 3. EXPERIMENTAL WORKS

The material of the workpiece – Table 1 - was the corrosion resistant steel, DIN 1.4404, X2CrNiMo1732 (equivalent standard AISI 316L), technical delivery terms EN 10088, dimensional and shape deviation tolerances according to EN 9445 with the austenitic structure, ground surface. These steel grades have increased corrosion resistance in chemical environments and are used for structural components, instruments and apparatus in the chemical industry. The blank rods  $\varnothing 30$  mm and 3,000 mm in length were machined to the  $\varnothing 29$  mm and 15 mm in length.

The workpieces were mounted to a special precise fixture with a ground screw acting on the top of the specimen wall to prevent radial deflections. The whole assembly was coaxially fixed to the dynamometer KISTLER 9272, fully controlled with a computer.

The dynamometer set was placed into the new CNC machining centre MCV 1210 (ZPS TAJMAC, share company, Zlin) controlled with the Sinumerik 840D. Kistler dynamometer 9272, charge amplifiers 9011 and the Dynoware program for force and torque analyses of the sample loading were used. The sampling rate 3kHz, low-pass filter and the long time constant were set for all data acquisition. A special CNC programme was written for automatic control of the reaming operation and the canned cycles.

The following technological sequence of tools was set:

- short helical carbide center drill  $\varnothing 6.4$  mm, Guhring, Art. Nr. 736, HSK - A63 D17356) for the center hole drilling,
- solid carbide drill  $\varnothing 8$  mm, thermogrip Bilz – HSK A63  $\varnothing 8$  ( $v_c=60$  m/min,  $f=0.1$  mm) – the pilot hole,
- whole carbide drill M44  $\varnothing 17$  mm, tool holder Weldon HSK – A63 D18 A80 CFB-01, ( $v_c=60$  m/min,  $f=0.1$  mm) – boring operation,

- monolithic boring bar HF, carbide inserts CCMT 060204  $\phi 17.7+0.05$  mm, tool holder HSK A63 D16 A100 – DFB01 ( $v_c=60$  m/min,  $f=0.1$  mm),
- countersink  $90^\circ \phi 30$  mm, DIN 335, Guhring, Art. Nr. 327 tool holder - thermogrip Bilz – HSK A63  $\phi 20$
- monolithic cermet reaming head MT3 HAM FINAL Ltd.,  $\phi 17.814$  mm, coated with the nanocomposite super-nitride (Ti<sub>0.4</sub>,Al<sub>0.6</sub>)N, CemeCon HYPERLOX, gripped in the carbide thermogrip HAM-FINAL. The Fuchs Oil emulsion ECOCOL 68 CF2 (10% concentration, 60 bars in pressure, flood intensity 50 l/min) and outer system of cooling with an emulsion reservoir of 1,200 litres for the machining were used. The temperature of the cooling fluid as measured during all machining and it was changing in the range of 20-25°C. Cutting speed  $v_c=40-100$  m/min,  $a_p=0.057$  mm,  $f=0.2-0.8$  mm were tested. Two reamer heads have been tested for statistically pooled data assessment.

Chemical composition (weight %)				
C	Si	Mn	P	Ni
0.016	0.39	1.4	0.027	11.21
Cr	Mo	S	N	Fe
17.31	2.11	0.026	0.052	rest
Mechanical properties				
Yield point $R_e$ [MPa]	Tensile strength $R_m$ [MPa]		Dilatability - $A_{80 \text{ min.}}$ [%]	
240 - 270	530 - 680		40	

Tab. 1. Composition and properties of the tested material

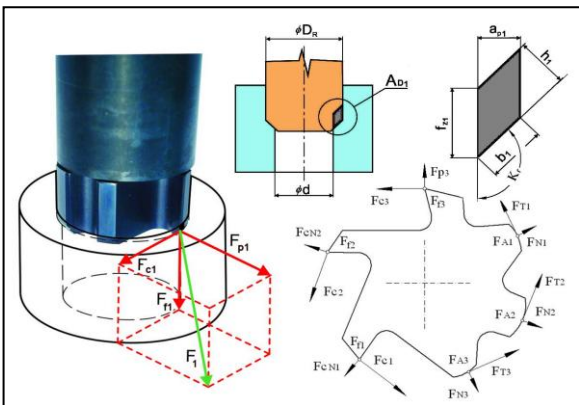


Fig. 1. A model of a reamer force loading, a chip cross-section

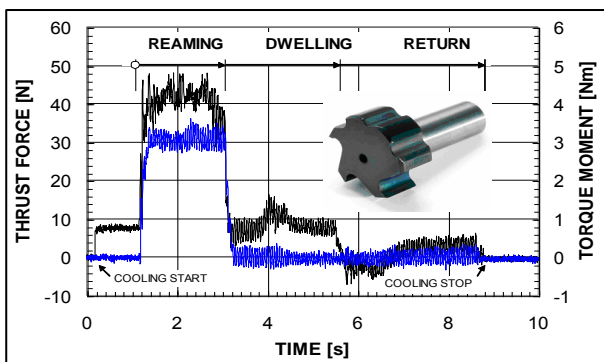


Fig. 2. Time series of the measured torque and thrust force

The statistically assessed results can be seen in Fig. 3, 4.

**4. CONCLUSION**

The nanocomposite super-nitride (Ti<sub>0.4</sub>, Al<sub>0.6</sub>)N coating efficiently protected the reamer heads for finishing of austenitic stainless steels. The accuracy of IT5, roughness Ra<1.0  $\mu$ m and other beneficial phenomena can be achieved even in very intensive cutting conditions for machining of the austenitic stainless steel. However, a very effective flood cooling with enriched cutting emulsion should be used and analyzed more.

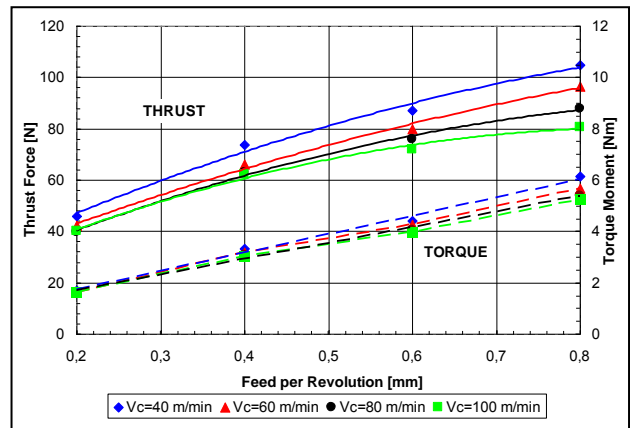


Fig. 3. Torque and thrust as functions of feeds and cutting speeds when reaming (pooled average values)

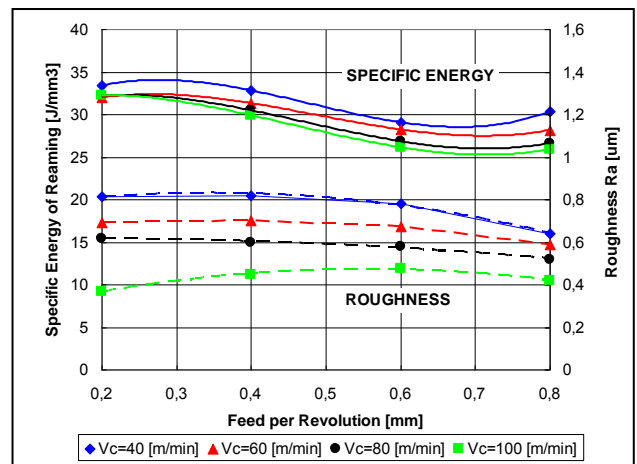


Fig. 4. Specific energy and roughness as functions of feeds and cutting speeds when reaming (pooled average values)

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\*\*\* ISO 3002-4 (Basic Quantities in Cutting and Grinding -Part 4: Forces, energy, power).